

Press fitting systems for saturated steam plants





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1.0 Steam distribution plants

1.1 What is the steam?

A fluid is in a saturated steam state when:

- the liquid phase and the vapour phase are in equilibrium with one another;
- in this condition, the number of particles passing from the liquid phase to the gaseous phase are equal to the number of those that condense into the liquid.

Water is the liquid referred to in this manual, to be transformed into saturated steam.

1.2 Processes where saturated steam is used

In industrial environments, steam plants are used in very large quantities.

Among the many applications, we summarize below some of the most classic uses:

- electricity generation in thermoelectric power plants;
- production of pulp and paper;
- petrochemical industry;
- food industry such as dairy products, bakery products, pasta, oilseeds, confectionery, cured meats, processing and packaging. Production processes such as blanching, peeling, baking, distillation, pasteurisation, cellophane dehydration are some of the most common productive phases where the steam is used;
- refining of sugar;
- beverage and foodstuff bottling lines for the cleaning and sterilisation of containers;
- pharmaceutical, hospital and medical sectors: in the medical field, thermal sterilisation of materials and equipment (a typical operating temperature of 165°C) is essential for keeping instrumentation under sterile conditions;
- Iaundry and ironing: in these applications, the typical operating temperature is 135°C for process water heating and for raising the humidity level.





1.3 Steam as a heat transfer fluid

At the theoretical level, any fluid can be used as a heat transfer fluid. However, fluid that accumulates and transfers heat must have some characteristics to allow it to be used in the industrial environment.

The main characteristics a fluid must possess to transfer heat are as follows:

- not be dangerous: the fluid should not be a direct or indirect source of danger. The choice therefore excludes flammable, toxic and radioactive fluids, and all fluids in general that require dangerous working phases;
- be economical: large-scale industrial use requires that the cost of the fluid that accumulates and transfers heat and the required facilities including maintenance and management are as low as possible;
- **D** not be corrosive: the fluid must not be corrosive to pipes, tanks and equipment;
- present a high coefficient of heat exchange: the higher the coefficient of heat exchange, the smaller the exchange surfaces;
- present high heat transfer capacity: with equal thermal power, the flow rates are reduced.

Notwithstanding the above, the saturated steam generated by water is the most suitable fluid for accumulating and transporting heat.

The only hazard associated with the use of steam is in relation to the pressure and temperature at which steam is produced and distributed.

1.3.1 The different grades of steam purity

Steam is classified according to the different grades of purity, which is why it is used in different application fields.

1.3.2 Plant steam

Plant steam is understood to be steam with the lowest qualitative grade and with the greatest potential for contamination. The factors influencing steam quality are:

- incoming water to the boiler is not purified;
- losing of chemical substances used in the plant and poor water treatment management;
- steam generator management with control of load, levels, dissolved salt solutions, operating parameters (pressure, temperature, etc.);
- the contamination resulting from other production processes.

Industrial steam is characterised by the presence of additives such as anti-corrosive agents, high pH, and relatively high operating pressure (between 3 and 10 bar).

1.3.3 Filtered steam

Filtered steam is the typical steam classified as "culinary": it is produced from the plant steam through microfiltration using an extremely thin stainless steel element. Normally the filter has a 5 µm mesh to block solid particles and droplets of water. The use of filters does not eliminate the potential risk of contamination from the extraction of impurities from the boiler and cross contamination.

The amount of contaminants that can be detected downstream of the filter is due to many factors including the maintenance regime and the speed of the steam flow.



1.3.4 Clean steam

Clean steam is the grade of steam purity that is used for sterilisation in hospital environments, for food and beverages.

Clean steam is generated from decontaminated water in a dedicated steam generator. IT is free of low pH additives (between 5 and 7) and is produced and distributed at low pressures (max. 3 bar).

When it comes to "clean" steam, we refer to UNI EN 285:2016, which specifies the requirements and tests for large steam sterilisers, essentially used in sanitary sterilisation for medical devices and their accessories.

1.3.5 Pure steam

Pure steam is the evolution of clean steam aimed at the pharmaceutical industry and biotechnology. The characteristics of purity and quality found in pure steam are in fact beyond what is required by current legislation concerning the food and beverage industry.



Classification of steam purity grades and their applications.

1.4 Water for steam production

The parameters of the water used for steam production are influenced by the type of steam you want to produce. These parameters should be periodically monitored to ensure the required quality.

The key parameters to be controlled are:

- oxygen and carbon dioxide are aggressive gases and cause corrosion: they are eliminated by thermal degassing;
- electrical conductivity, a body's ability to let an electric current flow: conductivity increases as the concentration of ions (dissolved salts) increases;
- In a sessing the possible formation of incrustations following salt precipitation;
- iron: the precipitation of iron ions generates incrustation and corrosion;
- PH: is the measure of acidity/basicity of water; it must be maintained by adding alkalinisers at an optimum value of 9.0 to 9.3 to limit corrosion of the metals.



1.4.1 Industrial steam production

| General requirements | | colourless, transparent and free of suspended solid particles | | | |
|--|-----------------|---|----------------------------|--|--|
| pH value at 25°C | | > 9 | > 9 | | |
| Conductivity at 25°C | μS/cm | only guideline values deter | mined for the water supply | | |
| Sum of the alkaline-ferrous metals | mana al distana | < 0.01 | > 0.01 | | |
| (Ca ²⁺ + Mg ²⁺) | mmoi/intre | < 0.01 | 20.01 | | |
| Oxygen (O ₂) | mg/litre | 0.05 | ≥ 0.02 | | |
| Carbonic acid (CO ₂) composition | mg/litre | < 25 | < 25 | | |
| Total Iron (Fe) | mg/litre | < 0.2 | < 0.1 | | |
| Total copper (Cu) | mg/litre | < 0.05 | < 0.01 | | |
| Oxidisability (Mn VII ->Mn II) | | - 10 | < 10 | | |
| of which KMnO ₄ | ing/inte | < 10 | < 10 | | |
| Oil, grease | mg/litre | <] | <] | | |
| organic substances | - | see note 1 | | | |

For industrial steam production, filtered, colourless water is used with the characteristics listed in the table below, depending on the pressure of the generator (boiler).

Note 1 Organic substances are generally mixtures of different compounds. The composition of such mixtures and the behaviour of their components at operating conditions of the the boiler are difficult to envisage. Organic substances may decompose into carbonic acid or other acid products, which increase conductivity and cause corrosion and deposits. They can also cause foam and/or sediment formation, which must be minimised. Total TOC (Total Organic Carbon) content must also be minimised.

| General requirements | | colourless, transparent and free of suspended solid substances | | | | | |
|----------------------|------------|--|--------|-----------|--|--|--|
| pH value at 25°C | | 10.5 ÷ 12 10.5 ÷ 11.8 10 ÷ 11 | | | | | |
| Acidity | mmol/litre | 1 ÷ 12 | 1 ÷ 10 | 0.1 ÷ 1.0 | | | |

1.4.2 Pure steam production

Pure steam production is carried out through a stainless steel tubular heat exchanger where heating is carried out with industrial steam circulating within the casing.

Prior to use, the "pure" steam is conveyed to a chamber where the fluid slows down to avoid the condensation droplets being drawn to the users. Adopting this measure, "sterile" steam is obtained without additives and impurities.



1.5 Choosing the right steam type

Below is the logical path to follow for the correct choice of steam type to be used according to the production process.



(From ISPE Baseline Pharmaceutical Engineering Guide)



2.0 Saturated steam production plant components

The transformation of energy in the saturated steam plants is through a system consisting of the following 3 macro components:

- heat generator (boiler): this is the heart of the system. In it a solid, liquid or gaseous fuel is reacted with oxygen contained in the atmospheric air. From this chemical reaction of oxidation, heat is transferred to the heat transfer fluid (dry saturated steam) that will deliver heat to the users;
- distribution lines: the pipes allow the transfer of the heat transfer fluid from the generator to the users;
- in the user equipment, steam transfers the accumulated thermal energy to a second process fluid or to the working environment.



Production of pulp and paper



Pharmaceutical industry



Bottling line



Industrial plants





Steam pressure control systems

3.0 System components

3.1 Press fitting - product definition

A distribution system this well branched and widespread requires an innovative application solution. Forget installation procedures such as welding or threading.

The press fitting system is simple and requires only the automatic crushing of a pipe on a fitting, without welding, gluing or crimping. This new system is fast and cheap, because it requires only half the time for installation and therefore provides significant time savings.

A plant built with press fitting is very durable because the steel tubes are inherently tougher and more rigid.

The advantages offered by the **inoxPRES** press fitting system specifically designed for the production of steam plants are summarised in the following points:

- easy assembly, practical and convenient (efficient);
- Quick installation with savings on hours of labour;
- safe and approved (guaranteed system);
- no need for specialised personnel (no special skills required);
- safe and no use of naked flames.

These characteristics make the press fitting system particularly suitable for industrial applications (where technical regulations permit). Press fitting systems are an ideal solution for the production of steam circuits in view of the need to ensure the cleanliness of fluid flow. In addition, the **inoxPRES** range is the most suitable for the production of steam circuits: the fittings and piping are made of stainless steel, a "clean" material, highly resistant to corrosive processes and with high mechanical performance, without the risk of the fluid flow becoming contaminated. Reduced thickness with large cross section, drastically reduces load losses and allows higher flow rates and better performance than traditional systems.

The press fitting system is only designed for saturated steam and is not intended for applications with overheated steam.



3.2 Press fitting - inoxPRES: characteristics

The **inoxPRES** system is particularly efficient because it is made of AISI 316 (1.4404) stainless steel, among the best stainless steel alloys available, and has been tested and approved by the main international certification bodies.

| Pressure | | | | |
|-------------|---|--|--|--|
| Min | -0.95 bar | | | |
| Мах | PN 16 (16 bar) ø 15 mm up to ø 108 mm | | | |
| Temperature | | | | |
| Min | -20°C | | | |
| Мах | +250°C (resistance of white STEAM o-ring) | | | |

| | Pressure |
|-----|---|
| Мах | PN 7 (7 bar) ø 15 mm up to ø 108 mm |
| | Temperature |
| Max | +165°C (resistance of white STEAM o-ring) |

DIMENSION RANGE

ø 15 ÷ 108 mm

Standard in stock

The STEAM mix is compatible with hydrocarbons, oils, and other aggressive substances.

It is always necessary to evaluate compatibility for uses that are outside the transporting of industrial water and steam.



3.2.1 Press fitting – inoxPRES: fittings



inoxPRES press fittings are manufactured using high-alloyed austenitic stainless Cr-Ni-Mo steel AISI 316L (material number 1.4404).

The press fittings are indelibly marked with laser reporting the manufacturer name, diameter and internal code.

At the bulging ends of the press fittings a standard high temperature resistant white STEAM ring seal is inserted, specifically designed for saturated steam applications.

The range of press fittings is available with figures that have threaded terminals according to the standard EN 10226-1 (ex ISO 7/1).

The threading is suitable for sealing on the thread using teflon/hemp and where the following characteristics exist:

- conical male thread;
- cylindrical female thread.

3.2.2 Press fitting – inoxPRES: pipes

inoxPRES piping, with thin seamless walls, are made of high-grade austenitic stainless steel Cr-Ni-Mo AISI 316L (material no. 1.4404). The tubes are manufactured according to EN 10217-7 and EN 10312. Inner and outer surfaces are made of smooth metal and are free of corrosion-promoting substances. **InoxPRES** pipes are classed as a non-flammable material belonging to fire class A. They are supplied in 6m bars, the ends of which are closed with plastic caps.

| TABLE 4: INOXPRES PIPES - DIMENSIONS AND CHARACTERISTICS | | | | | | |
|--|---------------------------|----------------------------|--------------|---|--|--|
| EXTERNAL DIAMETER X THICKNESS mm | NOMINAL DIAMETER DN | INTERNAL DIAMETER mm | MASS kg/m | STEAM CONTENT 165 °C / 7 bar I/m | | |
| 15 x 1 | 12 | 13 | 0.351 | 0.038 | | |
| 18 x 1 | 15 | 16 | 0.426 | 0.058 | | |
| 22 x 1.2 | 20 | 19.6 | 0.624 | 0.087 | | |
| 28 x 1.2 | 25 | 25.6 | 0.790 | 0.149 | | |
| 35 x 1.5 | 32 | 32 | 1.240 | 0.232 | | |
| 42 x 1.5 | 40 | 39 | 1.503 | 0.345 | | |
| 54 x 1.5 | 50 | 51 | 1.972 | 0.590 | | |
| 76.1 x 2 | 65 | 72.1 | 3.550 | 1.176 | | |
| 88.9 x 2 | 80 | 84.9 | 4.150 | 1.639 | | |
| 108 x 2 | 100 | 104 | 5.050 | 2.453 | | |



| TABLE 5: MECHANICAL CHARACTERISTICS INOXPRES PIPES | | | | | |
|--|---------------------------------|--|--|--|--|
| Tensile strength | 600 N/mm ² | | | | |
| Yield strength | 220 N/mm ² | | | | |
| Elongation | 40% | | | | |
| Linear expansion coefficient | 1.7 x 10⁻⁵ | | | | |
| Surface roughness | ≤1.0 µm | | | | |
| Fire resistance | according to DIN 4102-1-Class A | | | | |

3.2.3 Press fitting – inoxPRES: seals

Traditional press fitting systems use round sealing rings (O-rings), which can easily be damaged in the event of unsuitable processing.

RM on the other hand uses a patented sealing ring with a lenticular profile which fits the press crimp groove. This provides the following advantages:

a 20% enlargement of the sealing surface area;

- significant reduction in the risk of damage to the sealing ring;
- easy pipe insertion.

The steam sealing ring is a special STEAM mix, that is white (\emptyset 15÷108 mm) and resistant to high temperature, specially designed for the conveyance of steam.

The excellent mixing characteristics allow the o-rings to withstand **saturated steam up to a temperature of 165°C**, **maximum pressure of 7 bar.**







The **inoxPRES** range offers several solutions to facilitate different plant situations.





4.0 Design of the steam transport network

The dimensioning of the steam ducts requires knowledge of the following parameters:

- steam flow rate;
- > thermodynamic conditions of the steam.

The dimensioning and management of the system must be achieved by reducing the load losses as much as possible. At the design stage, the basic parameters to be addressed are:

- fluid speed;
- the size of pipelines;
- the slope of the lines.

4.1 Fluid speed

The maximum permissible speed of the **dry saturated steam** must be maintained at around 10 m/s (<25 m/s) for all pipes with a diameter of up to 5"-6".

4.2 Piping dimensioning

The pipes are sized starting from the pressure required at the point of use under maximum flow conditions. After setting the speed value in the pipeline, it is possible to define the diameter of the pipeline and its relative load losses. In general, load losses must remain within the parameters shown below in table.

| P (bar) | Load loss (bar/100 metres) |
|---------|----------------------------|
| 0-2 | 0.1 – 0.3 bar |
| 2-10 | 0.3÷1 bar |

When the supply pressure is set, the constant load losses are established, to calculate the pressure at the point of use. Then the speed will be checked, which must be maintained within the parameters indicated in paragraph 4.1.



The design choices will have an effect in terms of cost and efficiency of the final result. Both in the event of oversizing and undersizing, there will be problems that are summarised in the table below.

| Oversized pipes | Undersized pipes |
|---|---|
| higher cost of piping than necessary | higher speed of steam |
| higher condensation volume | increased pressure drop |
| poor quality steam and thermal energy caused by condensation | pressure lower than that required at the point of use |
| higher thermal energy losses | insufficient steam volume at the point of use |
| | water hammering due to higher steam speed and greater risk of erosion |

In addition to the distributed load losses obtained from dedicated norms, concentrated load losses that are valued through specific tables should also be considered. For each component, the length of the equivalent pipeline is added to the piping considered for the distributed losses.

4.3 Expansion compensators

Straight tubular sections require the use of expansion compensators, fitted to prevent distortions to the pipes. The most widely used and recommended solution is the use of bellows expansion joints complete with guides. Compared to "omega" displacement compensators, they guarantee lower load losses and smaller dimensions.

4.4 Condensate discharge

The pipes must always be installed with an appropriate slope to the point of use, to facilitate the discharge of the condensate that is being formed.

Diameter reductions must always be performed using eccentric reducers to avoid condensation stagnation inside the piping.

The drainage of the condensate at the various points of the plant, prevents stagnation and consequent water hammering (overpressure caused by the impact of condensate against an obstacle). Possible water hammering in the system can cause the breaking of filters, valves and components.



RIDUZIONI DI DIAMETRO SU TUBAZIONI VAPORE



The different drainages must be maintained at appropriate distances to discharge the condensate: an approximate distance of 30 - 50 meters must be observed between one drainage point and the next.



4.5 User bypass

The bypass junctions at the top of the piping allows for the release of steam which is as dry as possible, without condensation residues that remain at the bottom of the main pipe.

In the event that decompression was carried out laterally or on the lower side, the condensate would enter directly into the equipment with the relative supply of "wet" steam .

In the same way as the main line, also with the bypasses, it is necessary to provide drainage points with a relative automatic discharge device, suitably positioned downstream of the extraction point.



4.6 Slope of the pipes / uphill path sections

As far as possible, it is always preferable to use a continuous slope of the pipes which produces less load loss. In cases where this is not possible due to structural obstacles, it is possible to return to the height through vertical uprights, then proceed again with the sloping section towards the extraction point.





PREVENTION OF WATER HAMMERING

When this configuration is not feasible, proceed with an upward-facing pipeline, opposed to the flow created by the steam movement.

In the inclined upward section, it is necessary to keep the speed low and check that the pipe diameter is of the appropriate diameter so that the steam speed does not exceed 15 m/s.

In addition, in the inclined section, the distance between the two subsequent condensate drainage points should be kept at no more than about 15 m. This is to prevent the condensate from rising inside the tubing.





4.7 Thermal insulation

The piping of the distribution network must be thermally insulated to minimize heat dissipation and condensation formation.

5.0 Pipe fixing, distances between clamps

Pipe supports serve to fix the pipe to the ceiling or wall and should compensate for changes in length which result from temperature variations. Through the setting of fixed and sliding points the length variations in the pipe are steered in the required direction. Pipe supports must not be mounted on fittings. Sliding supports must be so positioned that they do not prevent the piping from moving.

The maximum permitted support distances for press fitting pipes are shown in table 8.

| TABLE 8: MAXIMUM PERMITTED DISTANCES BETWEEN SUPPORTS | | | | | | |
|---|--------------------------------|--|---------------------------|--|--|--|
| DN | External pipe diameter (mm) | Distances between supports (m) DIN 1988 | Indicative values: (m) | | | |
| 12 | 15 | 1.25 | 1.50 | | | |
| 15 | 18 | 1.50 | 1.50 | | | |
| 20 | 22 | 2.00 | 2.00 | | | |
| 25 | 28 | 2.25 | 2.50 | | | |
| 32 | 35 | 2.75 | 2.50 | | | |
| 40 | 42 | 3.00 | 3.00 | | | |
| 50 | 54 | 3.50 | 3.50 | | | |
| 65 | 76.1 | 4.25 | 4.00 | | | |
| 80 | 88.9 | 4.75 | 4.50 | | | |
| 100 | 108 | 5.00 | 5.00 | | | |



6.0 Expansion compensation

Metal pipelines expand in different ways under the influence of heat and according to the material they are made of. The longitudinal change under various temperature differences in the **inoxPRES** press fitting pipe is shown in table 9. The longitudinal change can be compensated for through the correct setting of fixed and sliding points, the installation of compensators, s-bends, u-bends or expansion compensators and by the creation of sufficient expansion spaces. Typical installations are shown in the figures on page 19.

| | TABLE 9: INOXPRES LENGTH VARIATION | | | | | | | | | | |
|------------|------------------------------------|--------|------|------|------|------|------|------|------|------|------|
| | 1.5-1 | Δt[°K] | | | | | | | | | |
| | L[W] | 70 | 80 | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 160 |
| | 1 | 1.2 | 1.3 | 1.5 | 1.7 | 1.8 | 2.0 | 2.1 | 2.3 | 2.5 | 2.6 |
| | 2 | 2.3 | 2.6 | 3.0 | 3.3 | 3.6 | 4.0 | 4.3 | 4.6 | 5.0 | 5.3 |
| | 3 | 3.5 | 4.0 | 4.5 | 5.0 | 5.4 | 5.9 | 6.4 | 6.9 | 7.4 | 7.9 |
| | 4 | 4.6 | 5.3 | 5.9 | 6.6 | 7.3 | 7.9 | 8.6 | 9.2 | 9.9 | 10.6 |
| | 5 | 5.8 | 6.6 | 7.4 | 8.3 | 9.1 | 9.9 | 10.7 | 11.6 | 12.4 | 13.2 |
| | 6 | 6.9 | 7.9 | 8.9 | 9.9 | 10.9 | 11.9 | 12.9 | 13.9 | 14.9 | 15.8 |
| RES | 7 | 8.1 | 9.2 | 10.4 | 11.6 | 12.7 | 13.9 | 15.0 | 16.2 | 17.3 | 18.5 |
| Ä | 8 | 9.2 | 10.6 | 11.9 | 13.2 | 14.5 | 15.8 | 17.2 | 18.5 | 19.8 | 21.1 |
| Î | 9 | 10.4 | 11.9 | 13.4 | 14.9 | 16.3 | 17.8 | 19.3 | 20.8 | 22.3 | 23.8 |
| | 10 | 11.6 | 13.2 | 14.9 | 16.5 | 18.2 | 19.8 | 21.5 | 23.1 | 24.8 | 26.4 |
| | 12 | 13.9 | 15.8 | 17.8 | 19.8 | 21.8 | 23.8 | 25.7 | 27.7 | 29.7 | 31.7 |
| | 14 | 16.2 | 18.5 | 20.8 | 23.1 | 25.4 | 27.7 | 30.0 | 32.3 | 34.7 | 37.0 |
| | 16 | 18.5 | 21.1 | 23.8 | 26.4 | 29.0 | 31.7 | 34.3 | 37.0 | 39.6 | 42.2 |
| | 18 | 20.8 | 23.8 | 26.7 | 29.7 | 32.7 | 35.6 | 38.6 | 41.6 | 44.6 | 47.5 |
| | 20 | 23.1 | 26.4 | 29.7 | 33.0 | 36.3 | 39.6 | 42.9 | 46.2 | 49.5 | 52.8 |

Elongation of the pipe

$\Delta L = L x \alpha x \Delta t$

- ΔL = linear expansion in mm
- L = pipe length in m
- α = linear expansion coefficient
 - **inoxPRES** α = 0.0165 mm / (m x °K)
- Δt = temperature difference in °K





Figure A - Wall penetration detail



Figure 36 - Expansion compensation (Bd) using T units

Expansion arm calculation for displacement (Figures B and C)

 $Bd = k x \sqrt{(da x \Delta L)} [mm]$

k = constant

inoxPRES = 45

da = outer diameter pipe in mm ΔL = linear expansion in mm



Figure B - Expansion compensation (Bd) using orthogonal shift



Figure D – U-bend expansion compensation $(Bd\Omega = Bd\Omega / 1.8)$

Calculation formula U bend (Figure D)

BdΩ = k x $\sqrt{(\text{da x } \Delta L)}$ [mm] or BdΩ = Bd / 1,8

k = constant inoxPRES= 25 da = outer diameter pipe in mm ΔL = linear expansion in mm





TABLE 10: CALCULATION OF THE EXPANSION REACH (Bd) inoxPRES

TABLE 11: EXPANSION ARM FOR U DILATOR (BdΩ) inoxPRES





7.0 Processing

7.1 Storage and transport

inoxPRES system components have to be protected against dirt and damage during transport and storage. The ends of the pipes are factory-fitted with plugs/caps to prevent dirt. The pipes must be stored in a cradle with a protective coating or protected with plastic material, so that they do not come in contact with other materials. Furthermore pipes and press fittings must be stored in an environment which is covered and protected from moisture exposure in order to prevent corrosion and/or oxidation of the surface.



Pipe cutting

Deburring of the pipe

7.2 Pipes - cutting to length, deburring, bending

The pipes should be cut to length using professional pipe cutters which are suitable for the material in use. Alternatively, fine-tooth hacksaws or suitable electric saws may be used.

Not permitted are:

- tools which cause over-heating of the material and tempering of colours during cutting;
- oil-cooled saws;
- flame cutting or angle grinders.

To avoid damaging the sealing ring when inserting the pipe into the press fitting, the pipe must be carefully deburred, both inside and outside, following cutting to required length. This can be carried out using manual deburring

7.3 Marking the insertion depth

Sufficient mechanical strength of the press fitting connection will only be achieved if the insertion depths shown in table 12 are adhered to. These insertion depths are valid for pipes or fittings with insertion ends (i.e. fittings without pressfit end) and must be marked using a suitable marking tool.

The marking of the insertion depth on the pipe must be



The pipes can be bent by means of conventional bending tools up to an outer diameter of 22 mm ($R \ge 3.5xD$). No tube hot bending allowed.



visible directly next to the press fitting groove following pressing. The distance of the marking on the pipe/fitting from the press fitting formed end may not exceed 10% of the required insertion depth, since otherwise the mechanical stability of the connection cannot be guaranteed.

| TABLE 12: INSERTION DEPTH AND MINIMUM DISTANCES | | | | | | |
|--|-------------|---------|---------|--|--|--|
| Pipe outside diameter mm | A (*) mm | D mm | L mm | | | |
| 15 | 20 | 20 | 60 | | | |
| 18 | 20 | 20 | 60 | | | |
| 22 | 21 | 20 | 62 | | | |
| 28 | 23 | 20 | 66 | | | |
| 35 | 26 | 20 | 72 | | | |
| 42 | 30 | 40 | 100 | | | |
| 54 | 35 | 40 | 110 | | | |
| 76.1 | 55 | 60 | 170 | | | |
| 88.9 | 60 | 60 | 180 | | | |
| 108 | 75 | 60 | 210 | | | |



Minimum insertion depth and coupling

(*) Tolerance: ± 2 mm

7.4 O-ring check of press fitting

Before assembly the sealing ring must be checked to ensure that it is lying in the pressing groove correctly and that it is clean and undamaged. If necessary, the sealing ring should be replaced.

Additionally, the fitter should check whether the ring in position is suitable for the special application, or whether it should be replaced with another sealing ring.

7.5 Making the press connection

Using light pressure and making a turning movement at the same time, press the pipe into the press fitting up to the marked insertion depth. If the tolerances are so narrow that additional force is required to insert the pipe into the press fitting, then water or soapy water may be used as a lubricant.

Oil and grease are not permitted for use as lubricants.

Pressing is carried out using suitable electromechanical/ electrohydraulic pressing tools and dimension-matching pressing jaws or collars/chains. Tested and approved pressing tools or pressing jaws/collars/chains are listed under table 13-14.



Marking the insertion depth



Checking O-rings



The matching pressing jaw is mounted in the pressing machine, or the appropriate collar/chain mounted on the fitting, depending on the dimensions of the press fitting. The slot of the pressing jaw/collar must be positioned exactly over the press fitting formed end.

Following pressing, the complete connection should then be checked to ensure that the work has been carried out correctly and that the insertion depth is correct.

The fitter should also ensure that all connections have actually been pressed.

Following completed pressing, the pressing points may not be subjected to further mechanical loading. The positioning and straightening of the pipes and the sealing of threaded connections must therefore take place before the pressing is carried out. Slight movement and lifting of pipes, for example for painting work, is permitted.



Inserting the pipe into the press fitting



Assembly

7.6 Pressing tools

7.6.1 Basic indications

Pressing tools basically consist of the pressing tool and pressing jaws or collars/chains. Many of the pressing jaws/collars can generally be used with the pressing machines from one manufacturer. Additionally, many manufacturers of pressing tools have standardised the jaw attachment so pressing jaws from other manufacturers can also be used.

Press fittings in dimensions 15–35 mm must by pressed with jaws, 42–108 mm must by pressed with pressing collars/ chains.

Principally, all metallic press fitting systems have a pressing contour on the press fittings which matches the profile of the pressing jaws/collars. For this reason it is necessary to have the approval of the tooling by the manufacturer of the press fittings intended for use. In addition, it is important to follow exactly the maintenance and servicing instructions issued by the pressing tool manufacturer.



Klauke UAP3L





Novopress ACO2O3



Novopress ACO401



7.6.2 Approved pressing tools

RM approves the tools produced by Klauke and Novopress listed in the tables 13 and 14 below. These are pressing tools with the appropriate pressing jaws or collars/chains.

| TABLE 13: MANUFACTURER KLAUKE | | | | | | | | |
|-------------------------------|----------|--------------------|--------------------|-----------|---|--|--|--|
| Туре | | Piston strength | Dimension range | Weight | Compatible with jaws from | | | |
| MAP1 - MAP2L | | 15 KN | 15 ÷ 22 mm | ~ 2.5 Kg | | | | |
| UAP2 - UAP3L | | 32 KN | 15 ÷ 54 mm | ~ 3.5 Kg | Novopress EFP2 / EFP201 / AFP201 / EFP202 / AFP202 / EC0 1 / ACO 1 | | | |
| UNP2 | | 32 KN | 15 ÷ 54 mm | ~ 3.5 Kg | Novopress EFP2 / EFP201 / AFP201 / EFP202 / AFP202 / ECO 1 / ACO 1 | | | |
| UAP4 - UAP4L | | 32 KN | 15 ÷ 54 mm PN16 | ~ 4.3 Kg | Novopress EFP2 / EFP201 / AFP201 / EFP202 / AFP202 / ECO 1 / ACO 1 15 ÷ 54 mm | | | |
| UAP100 - UAP100L | | 120 KN | 76.1 ÷ 108 mm | ~ 12.7 Kg | | | | |
| | PKUAP3 | 32 KN | 15 ÷ 54 mm | ~ 12.3 Kg | Novonress | | | |
| AH- P700LS | PKUAP4 | 32 KN | 15 ÷ 54 mm PN16 | ~ 12.6 Kg | EFP2/EFP201/AFP201 / EFP202/AFP202 / EC01 / AC01 15 ÷ 54 mm | | | |
| | PK100AHP | 120 KN | 76.1 ÷ 108 mm | ~ 20.2 Kg | | | | |
| EHP2/SANB | | 0.75 KW | 76.1 ÷ 108 mm | ~ 69 Kg | | | | |

| TABLE 14: MANUFACTURER NOVOPRESS | | | | | | | |
|------------------------------------|--------------------|-----------------|----------|-----------------------------------|--|--|--|
| Туре | Piston strength | Range of use | Weight | Compatible with jaws | | | |
| ACO 102 | 19 KN | 15 ÷ 22 mm | ~ 1.7 Kg | | | | |
| EFP2 | 32 KN | 15 ÷ 54 mm | ~ 6.1 Kg | EFP 201 / AFP 201 / ECO 1 / ACO 1 | | | |
| EFP 201/EFP 202 | 32 KN | 15 ÷ 54 mm | ~ 4.4 Kg | EFP 2 ECO 1 / ACO 1 | | | |
| AFP 201/AFP 202 | 32 KN | 15 ÷ 54 mm | ~ 4.3 Kg | EFP 2 EC0 1 / ACO1 | | | |
| ECO 202/ACO 202 ECO 203/ACO 203 | 32 KN | 15 ÷ 54 mm | ~ 3.3 Kg | ECO 201 / ACO 201 ECO 1 / ACO 1 | | | |
| ACO 202XL ACO 203XL | 32 KN | 15 ÷ 54 mm PN16 | ~ 4.6 Kg | ECO 202 / ACO 202 | | | |
| AC0401 | 100 KN | 76.1 ÷ 108 mm | ~ 13 kg | | | | |
| ACO 3 | 36 KN | 15 ÷ 54 mm | ~ 5.0 Kg | ECO 3 | | | |
| ECO 301 | 45 KN | 15 ÷ 54 mm PN16 | ~ 5.0 Kg | ACO 3 | | | |
| HCP | 190 KN | 76.1 ÷ 108 mm | ~ 70 Kg | | | | |

GENERAL NOTE: only equipment with crimping force PN 16 must be used.



7.6.3 Periodical equipment service

Jaw and chain pressing units are to be serviced to guarantee a correct joint.

Press fitting tools must be checked by an authorised repair technician according to the manufacturer's specifications. Over and above any moving part (drive rolls) and pressing jaw and chain surfaces (internal profiles) are to be daily serviced, cleaned and lubricated.

All this is also indicated under UNI 7129-1.

Any possible oxidation, paint or dirt in general affect the tool reliability leading to equipment sliding problems on joints during pressing.



Klauke equipment

Keep the chain clean

لدوه



Novopress equipment







Keep the pins lubricated with oil

8.0 Testing and approvals

In accordance with European Directive 2014/68/EU (PED), saturated steam pipes with diameter \leq DN 100 used up to the maximum pressure of 7 bar/165°C, according to "Table 7" of the aforementioned directive fall into the class "Article 4 (3)" (no CE marking required, manufactured according to the proper construction practice in use in the manufacturing country).

The **inoxPRES** system with Steam sealing O-ring has passed tests under pressure with thermal cycles at the TTR Institute and has been used in several other field installations.

| | TTR INSTITUTE SRL Via Baden Powell 3/ter 21052 Busto Arsizio VA – Italy Tel.: +39 0331 342533 – Fax: +39 0331 342534 Reg. Imprese - Cod. Fisc P.Iva 03118550122 Capitale Sociale Euro 115.436,00 R.E.A. di Varese 324649 Pec: ttrinstitute.pec@legalmail.it |
|---|---|
| | Test report Nr: 1104859-001 |
| Customer: | Raccorderie metalliche Spa Strada Sabbionetana , 59 46010 Campitello di Marcaria (MN) Italia |
| test: reference std: | Thermal Cycles (STEAM) Internal Standard |
| Incoming sample: | 31-MAR-16 |
| Tested sample | INOXPRES Ø28 ASSEMBLY : INOXPRES FITTINGS / INOXPRES PIPE 316L O-RING STEAM |
| Raw material : | INOXPRES PRESSFITTING SYSTEM |
| Sampling : | to customer charge |
| Nr Fittings tested: | 19 FITTINGS |
| Order: | 26019270 |
| Date of test report: | 02-mag-16 |
| Note: | |
| The test report exclusive The test report must not Tested items will be ava | ely refers to the tested items. to be partially reproduced without the written approval of the laboratory responsible aliable for a period of 15 days after the test report date. |
| Date start test: | 29-mar-16 |
| | |







(EN 10204 - 2.1_ rev 0 of 04-2017)

relating to press fitting systems and stainless steel pipes

INOXPRES STEAM

RACCORDERIE METALLICHE S.p.A.

Strada Sabbionetana, 59 46010 Campitello di Marcaria Mantova (ITALY)

DECLARES

that the INOXPRES STEAM system press fittings and stainless steel pipes

- comply with UNI 11179 "Press fittings for metal pipes";
- comply with DVGW G5614 "Permanent pipe joints for metal gas pipes Compression fittings";
- comply with the requirements of the European Directive 2014/68/EU (PED: Pressure Equipment Directive);
- are suitable for the construction of networks for the delivery of saturated steam;
 - > maximum operating pressure 7 bar (PN 7);
 - > maximum operating temperature of +165 °C;
 - > conveyed fluid: saturated water steam;

The INOXPRES STEAM press fitting system and its components are manufactured under the Quality Management System Certificate ISO 9001:2008.

Campitello di Marcaria, April 2017

Ceccardi Guido Chief Executive Officer (CEO)

RACCORDERIE METALLICHE S.P.A. Sede e Stabilimento: Strada Sabbionetana, 59 - 46010 Campitello di Marcaria (MNI) Italy

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Partita IVA 01591820202 R.E.A. 169204







(EN 10204 - 2.1_ rev 0 of 04-2017)

relating to press fitting systems and stainless steel pipes

INOXPRES STEAM

CONFORMITY TO PED DIRECTIVE

The INOXPRES STEAM system press fittings and stainless steel pipes

- are suitable for the construction of networks for the delivery of STEAM with the following parameters;
 - > maximum operating pressure 7 bar (PN 7);
 - > maximum operating temperature of +165 °C;
 - > conveyed fluid: saturated water steam
- complies with the requirements of the European Directive 2014/68/EU (PED: Pressure Equipment Directive) Article 4, paragraph 3 for the dimensional range between Ø15 mm and Ø108 mm, for which no CE marking is required, having regard to the table for pipelines for the transport of fluids of Group 2, in particular steam.

To guarantee product quality and compliance with PED, the INOXPRES STEAM press fitting system and its components are manufactured under the Quality Management System Certificate ISO 9001:2008, which requires regular periodic checks on products and factory (third party inspection conducted by an independent body).

Campitello di Marcaria, April 2017

Ceccardi Guido Chief Executive Officer (CEO)

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INOXPRES STEAM

CORRECT USE OF THE SYSTEM

The INOXPRES STEAM press fitting system is suitable for steam installations with a maximum working pressure of 7 bar (PN 7) / maximum operating temperature of 165°C.

For correct use of the INOXPRES STEAM press fitting system, and successful installation please refer to the following documents:

Press fitting Technical Manual of Raccorderie Metalliche;

(on the website www.racmet.com the latest updated edition is always available)

- > European Directive 2014/68/EU (PED: Pressure Equipment Directive);
- > National regulations in force in the field of design, installation and maintenance of plants for transport of steam;

For the selection of pressing equipment, please refer to the Press fitting Technical Manual and use equipment declared compatible and suitable for use by Raccorderie Metalliche S.p.A.

Where required, the designer or installer must apply for the technical opinion of recognized body, which can approve the plant and choice of components installed.

Raccorderie Metalliche S.p.A. leaves it to the plant designer to assess the conformity of the INOXPRES STEAM press fitting system in accordance with territorial regulations and national laws that specify and regulate the design, installation and maintenance of systems intended for the transport of steam.

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INOXPRES STEAM

INOXPRES STEAM PRESS FITTING SYSTEM CHARACTERISITICS

Taking note of the following regulations:

- > Art. 7 Ministerial Decree 37 of 22-01-08 Rules for plant safety;
- > Art. 5 Law No. 447 of 06/12/91 Regulation implementing Law No. 46/90;

CERTIFIES

- that the INOXPRES STEAM system consists of press fittings, STEAM o- rings, connecting pipes, pressing tools and suitable clamps or chains;
- that the material used for the production of INOXPRES STEAM press fittings and pipes is AISI 316, 1.4404, in compliance with EN 10088 – EN 10312 – EN 10217-7;
- > that the INOXPRES STEAM press fittings are manufactured in compliance with UNI 11179;
- that all of the threads for the INOXPRES STEAM system are performed according to EN 10226-1 (DIN 2999 – UNI ISO 7/1) or UNI ISO 228/1 (DIN 259);
- that all the welds on the fittings for the INOXPRES STEAM system are 100% controlled, under pressure with automatic machines;
- > that the chloride content contained in the conveyed fluid, does not exceed 250 mg/l;
- that the STEAM seal can be used for saturated steam transport up to maximum working conditions P Max 7 bar / maximum temperature 165°C;
- that the INOXPRES STEAM system components are not subject to CE marking as prescribed by Legislative Decree no. 93 of 25 February, 2000;

Campitello di Marcaria, April 2017

| Ceccardi Guido | Pozzetti Silvio |
|-------------------------------|------------------------|
| Chief Executive Officer (CEO) | Head of Quality System |

Pizzamiglio Fabrizio

Product Manager Plumbing & Heating Division

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